

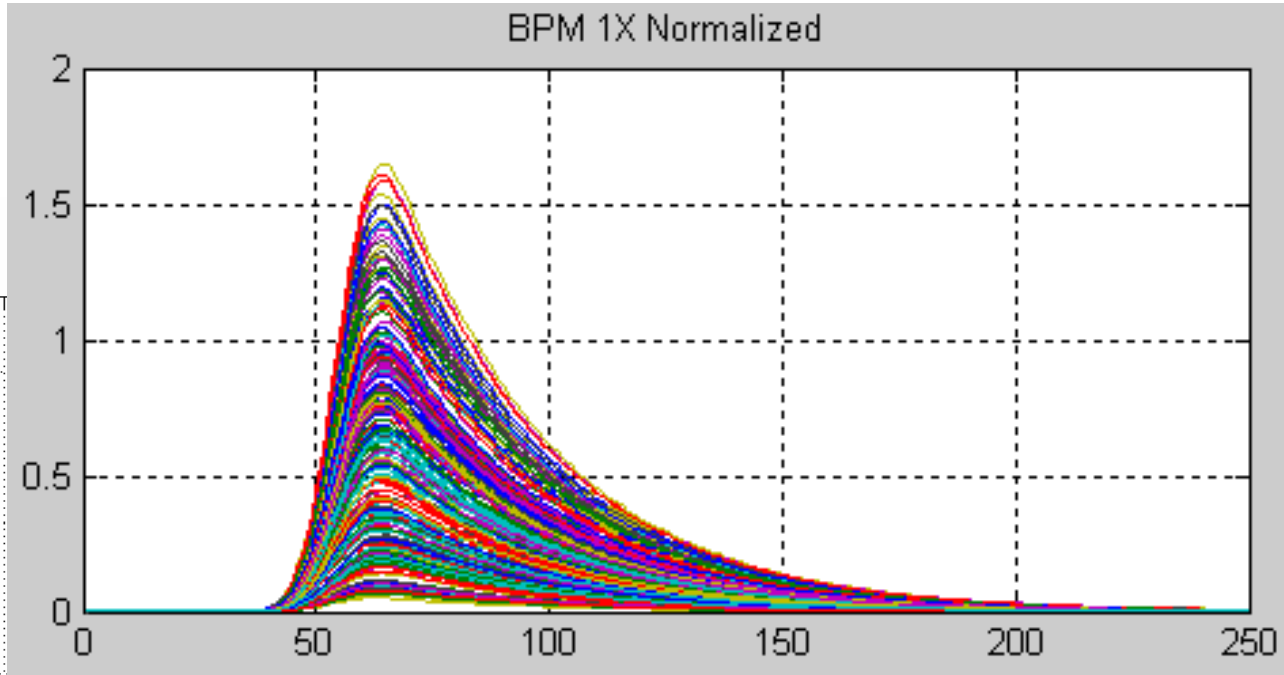
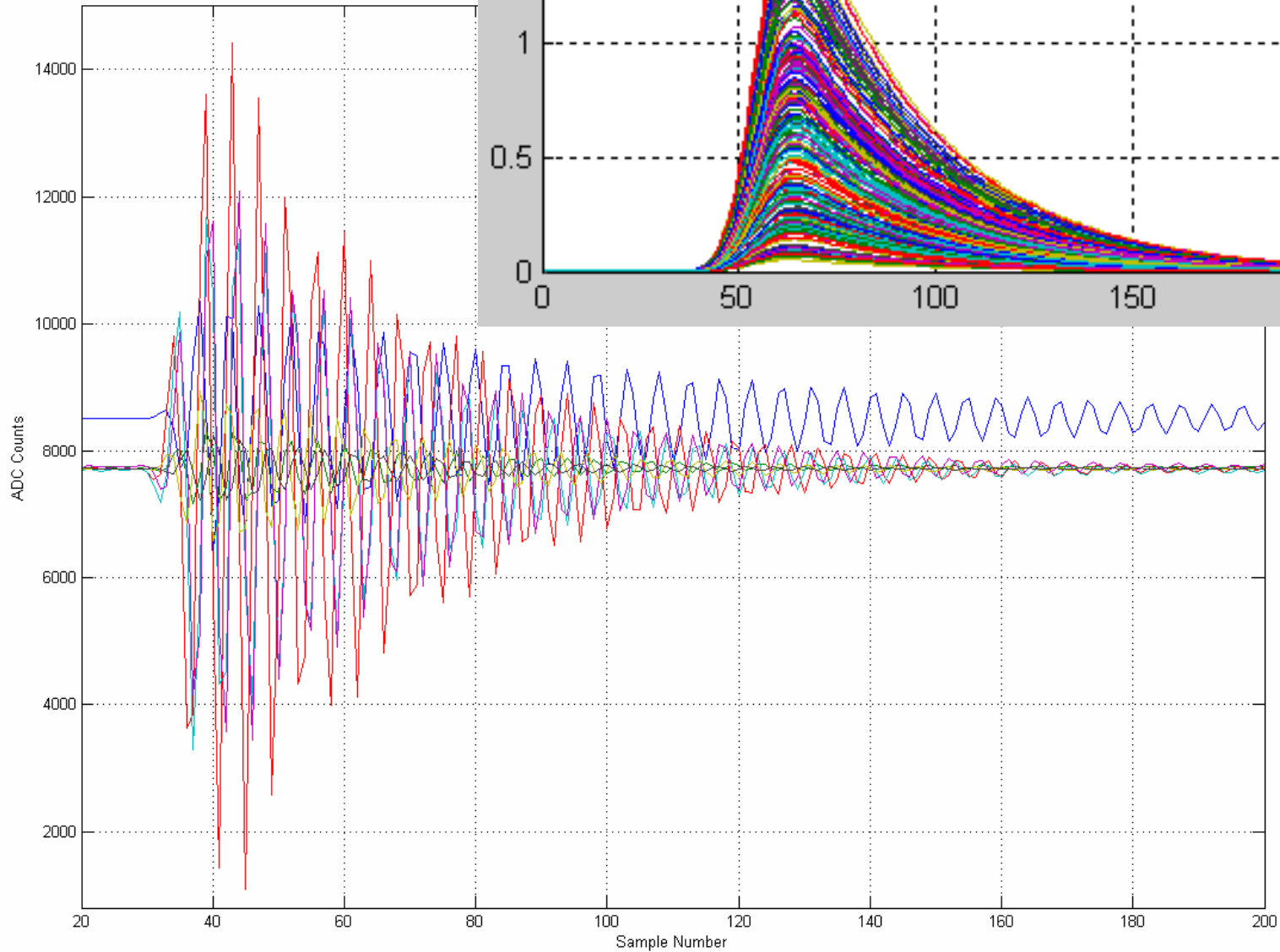
Digital Downconversion Processing Algorithm

nanoBPM Project
18 January 2005
Steve Smith

Cavity BPMs

- Position measurement is cavity dipole signal amplitude & phase.
- C-Band Cavities
 - First dipole mode frequencies are ~ 6426 MHz
- Dual Downconversion:
 - First IF at 476 MHz
 - Second IF at 25 MHz
- Digitize at 100 MSamples/sec
 - ~ 4 samples/ IF period
- Why don't we downconvert to baseband in analog to begin with?
- Digitizing at IF removes sensitivity to
 - Offsets
 - Low frequency noise
 - Gain differences (if (I,Q) down conversion is analog)

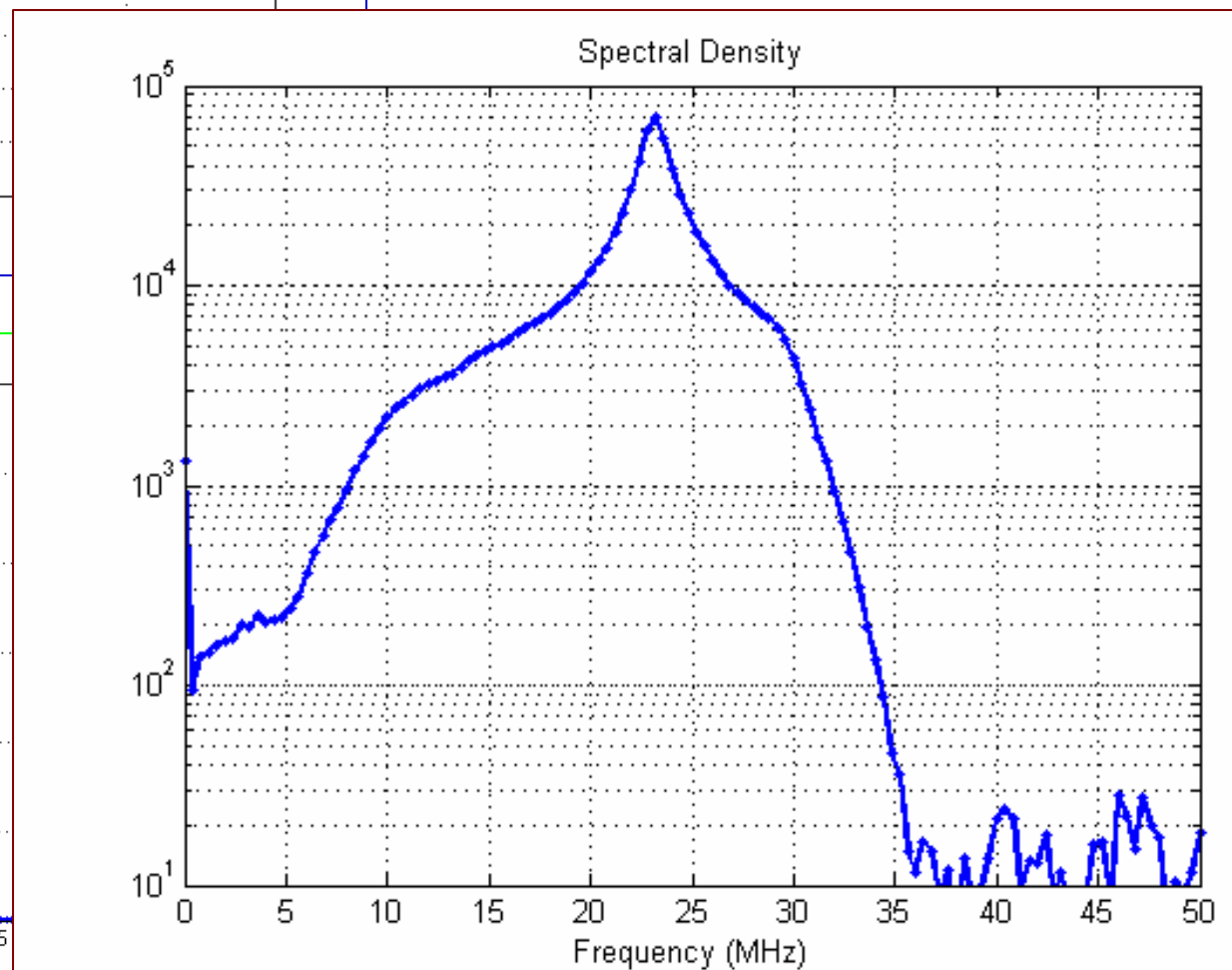
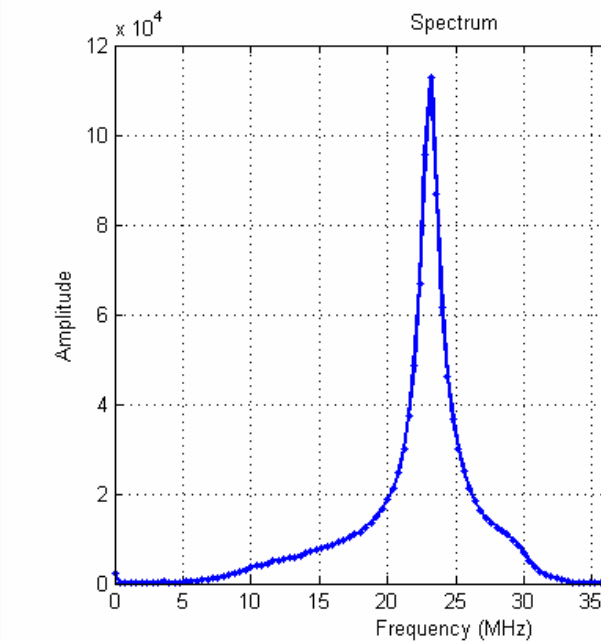
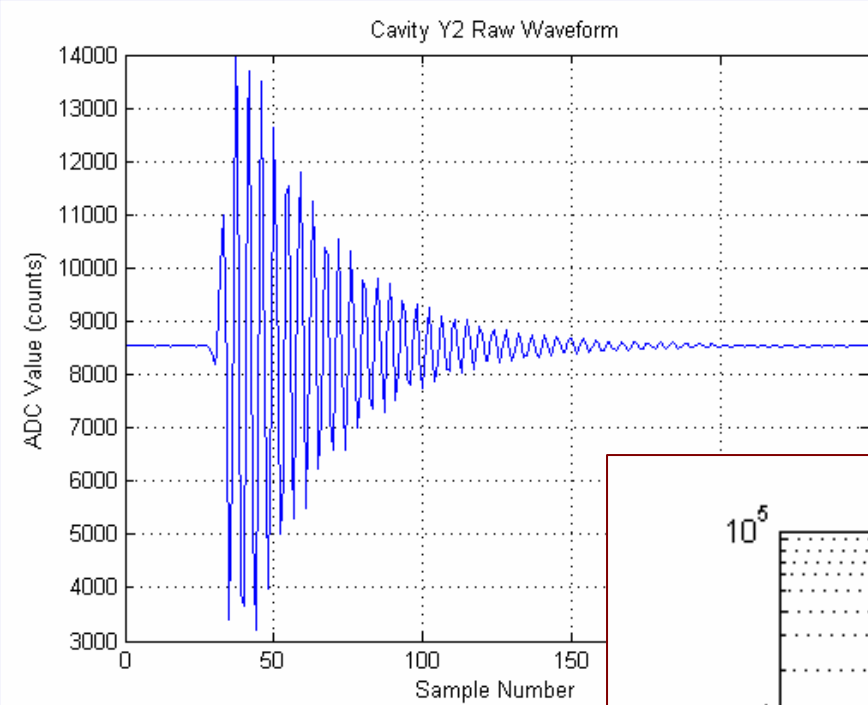
Data: Raw & Demodulated



Algorithm Overview

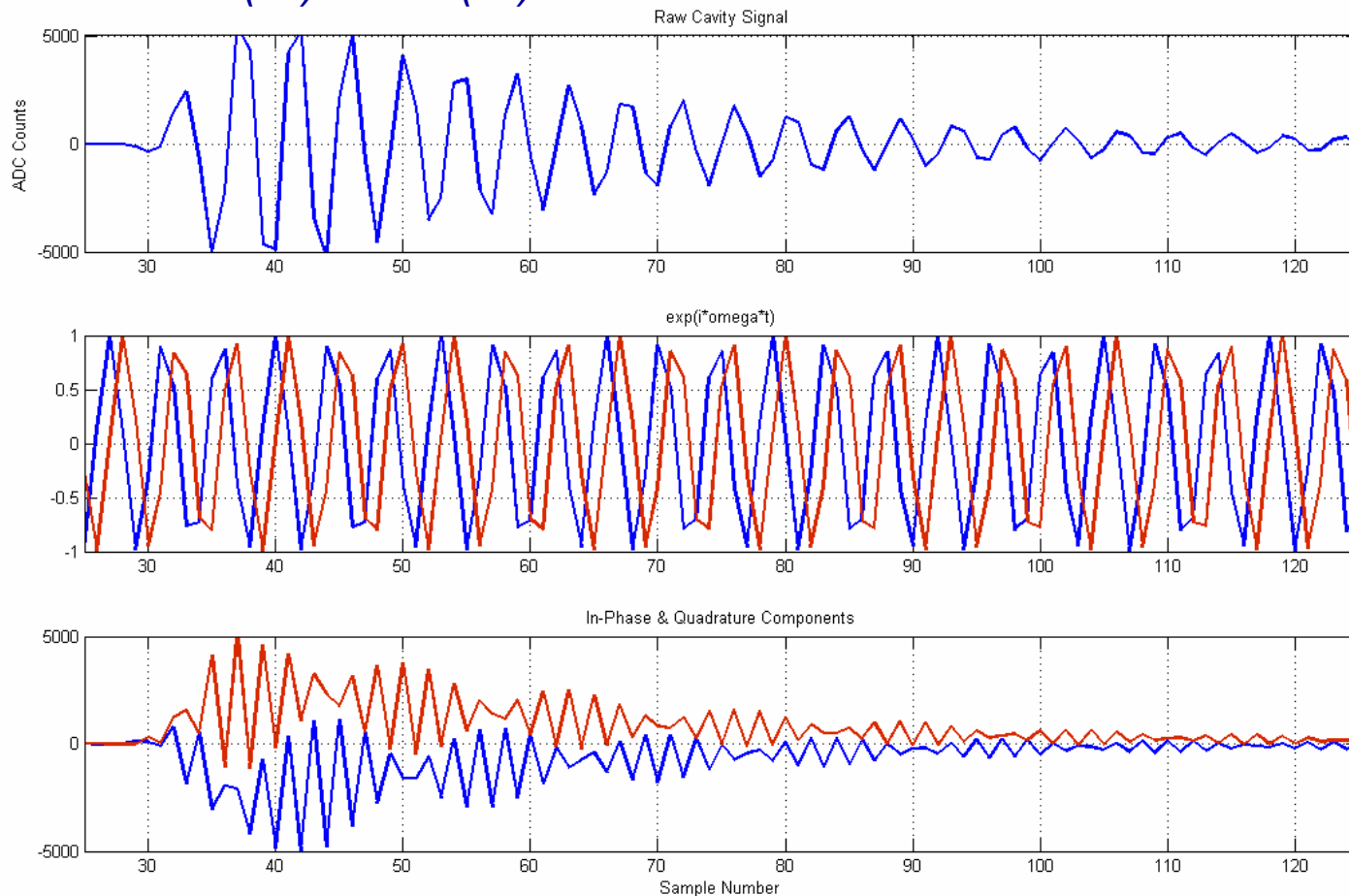
- Digitized IF
 - 14 bit ADC resolution
 - ~4 samples/ IF period
- Digital Downconversion:
 - Subtract approximate ADC zero
 - value not critical
 - Can use 1st sample or mean of first 20 samples, *et cetera*
 - Multiply digital waveform by complex "local oscillator" $e^{i\omega t}$
 - Low-pass filter (currently 2.5 MHz B/W)
- Sample complex amplitude of position cavity at "peak"
- Divide by complex amplitude from reference cavity
- Shift/Rotate/Scale by calibration constants

Cavity Signal Spectrum



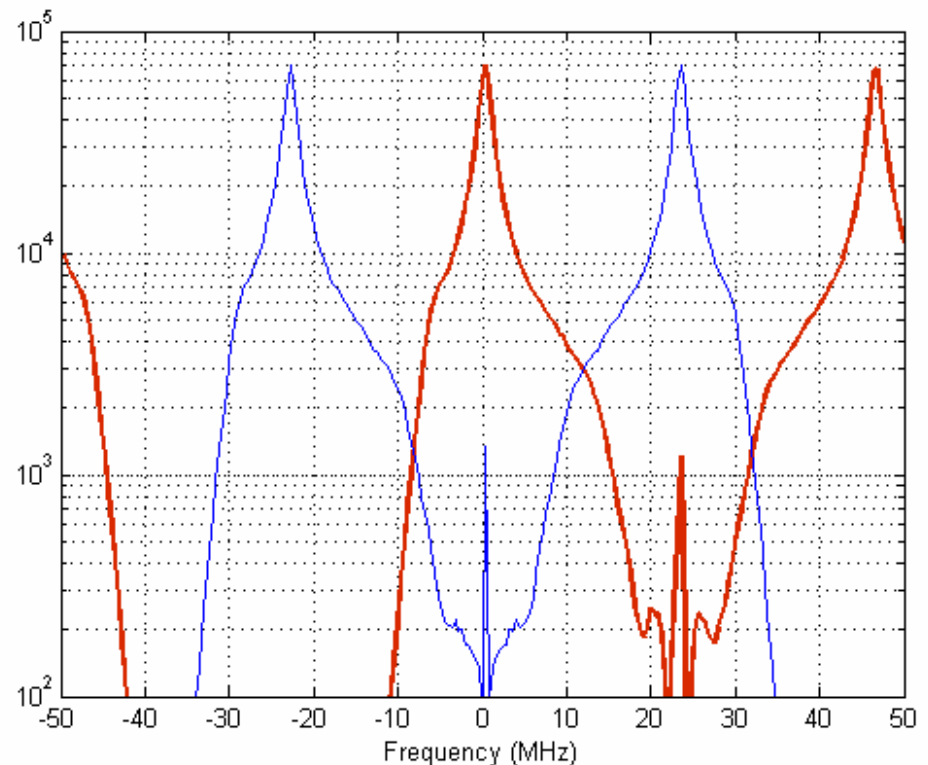
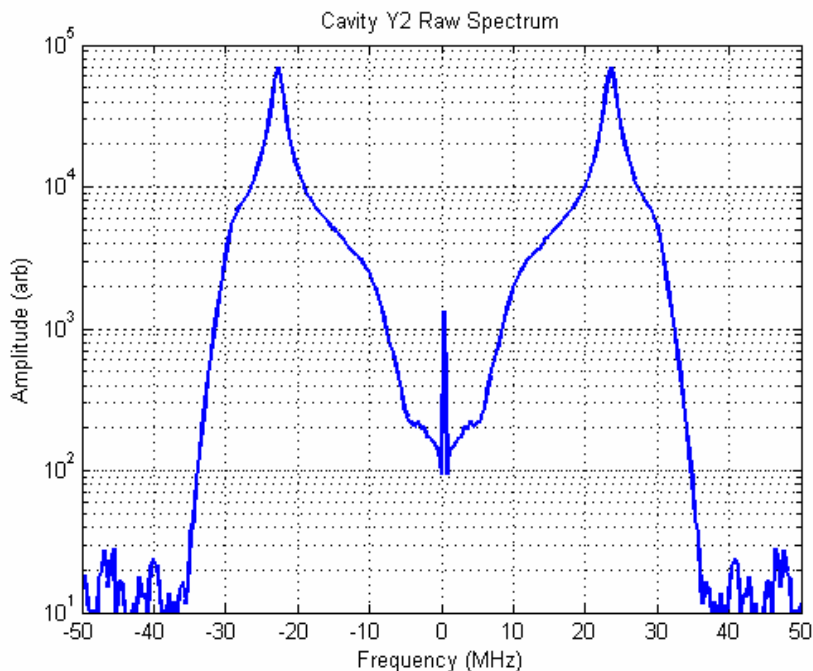
Digital Mixing

- Modulating by sine-like signal produces sum & difference frequencies:
 $\cos(\omega_1 t + \phi_1) * \cos(\omega_2 t + \phi_2) = (\cos((\omega_1 + \omega_2)t + (\phi_1 + \phi_2)) + \cos((\omega_1 - \omega_2)t + (\phi_1 - \phi_2)))/2$
- Don't pick out a particular phase yet,
 - keep phase information by multiplying by
 - $LO = \cos(\omega t) + i * \sin(\omega t) = e^{i\omega t}$

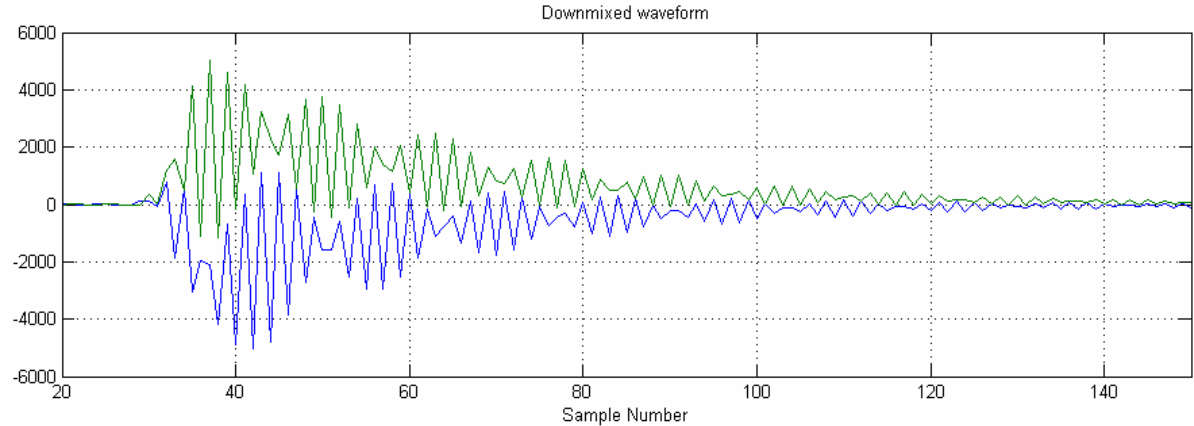


Digital Downconversion as Frequency Shift:

- $LO = \cos(\omega t) + i \sin(\omega t) = e^{i\omega t}$
- Think of this in either of two ways:
 - A convenient way of keeping track of the sine-like and cosine-like parts of the (real) signal
 - OR a frequency shift operator acting on the +/- frequencies of which the original signal was composed.
- Spectra
 - Raw signal (left)
 - multiplied by $e^{i\omega t}$ (right)



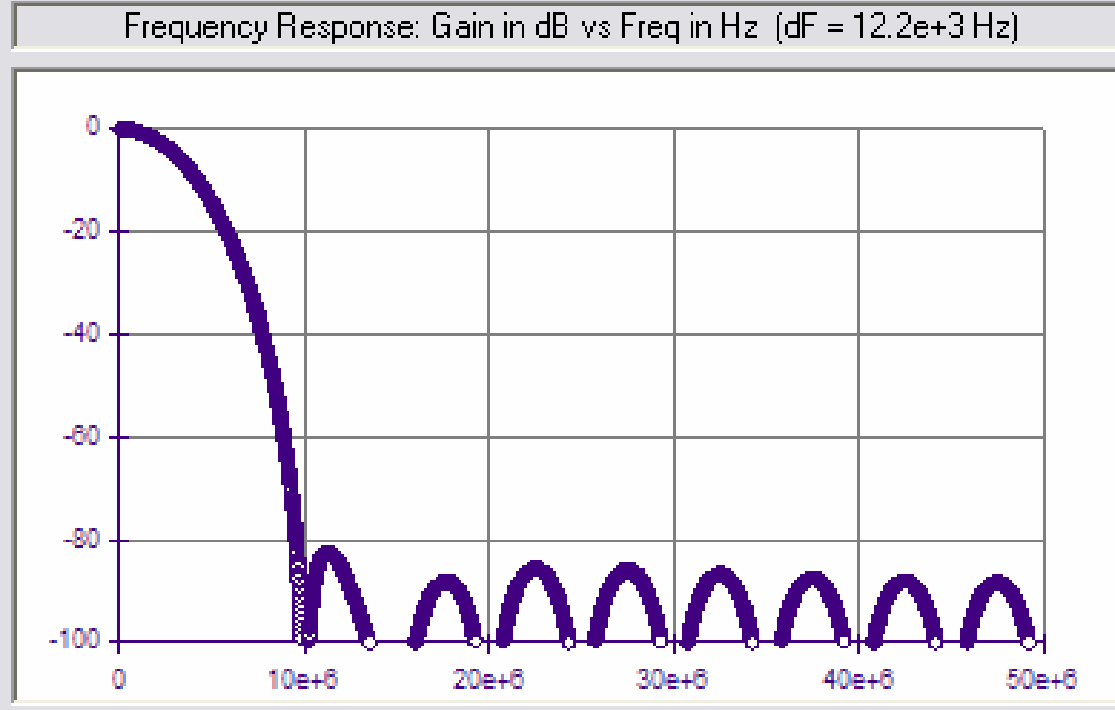
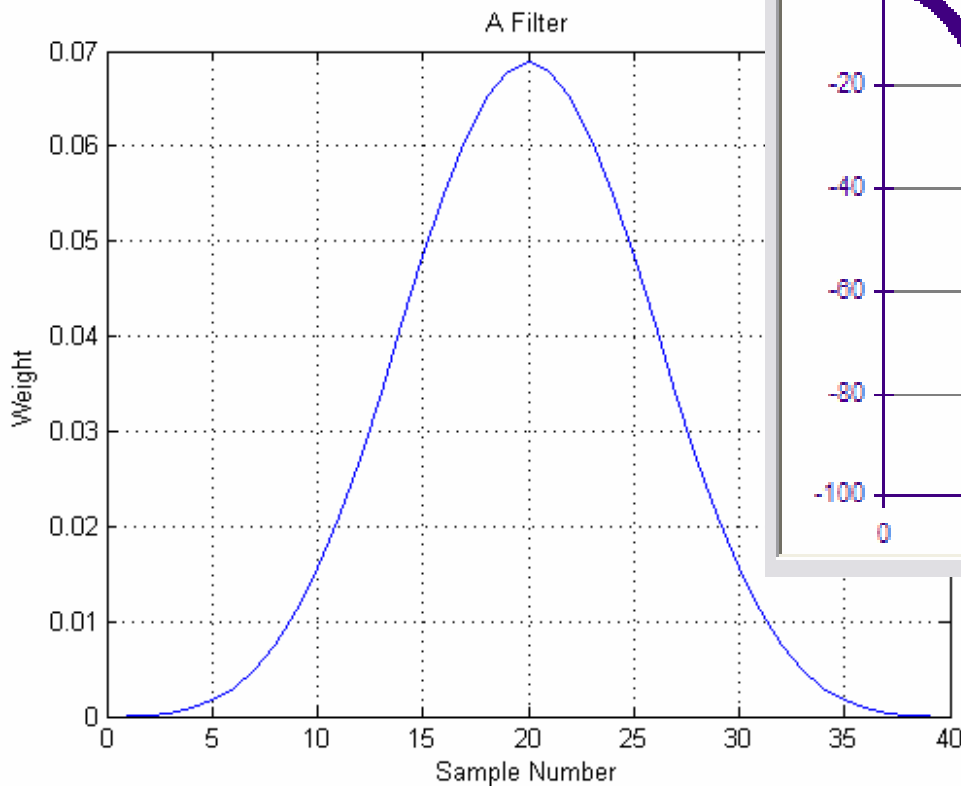
Filter



- Product is dominated by sum & difference frequencies
- Need a digital filter to remove
 - 2ω component (sum frequency)
 - (and ω component due to DC offset, low frequency noise)
 - other out-of-band noise
- Require:
 - lots of suppression at 2ω
 - Finite width in time domain
- Prefer
 - Quasi-Gaussian
 - Flat group delay (don't spread signal energy around in time)

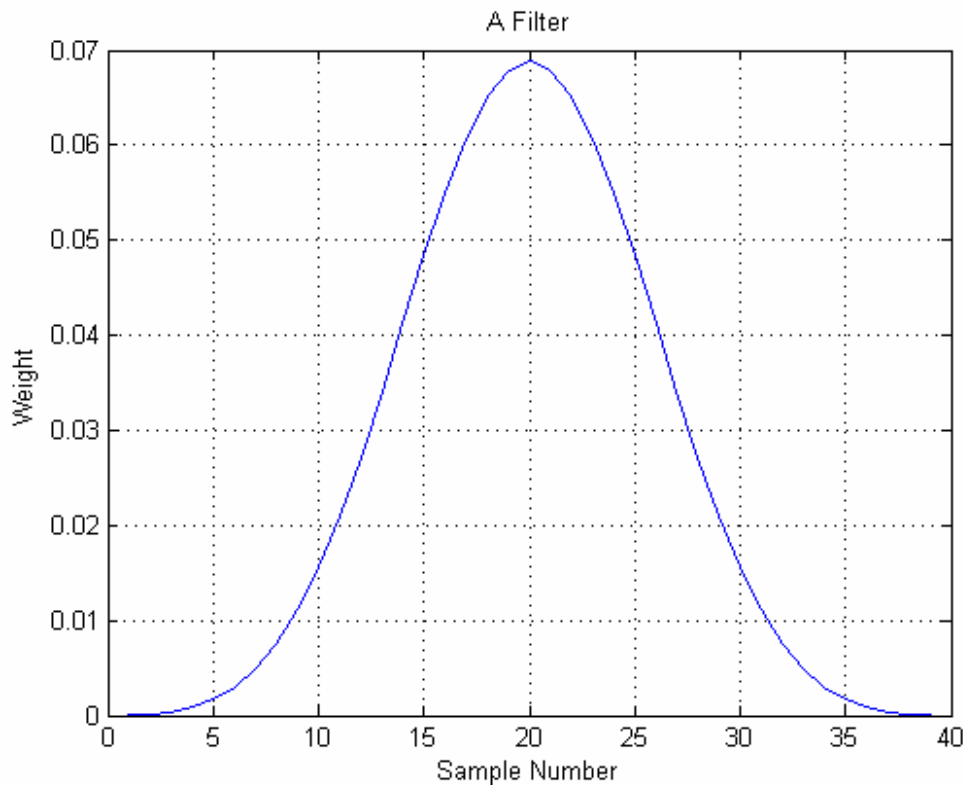
How to Describe a Filter

- Time domain
 - Vector of weights
 - Convolution with digitized waveform
- Frequency domain
 - Frequency response
 - Multiply with Fourier Transform of waveform
- Example:
 - 2.5 MHz - 39 Coefficients



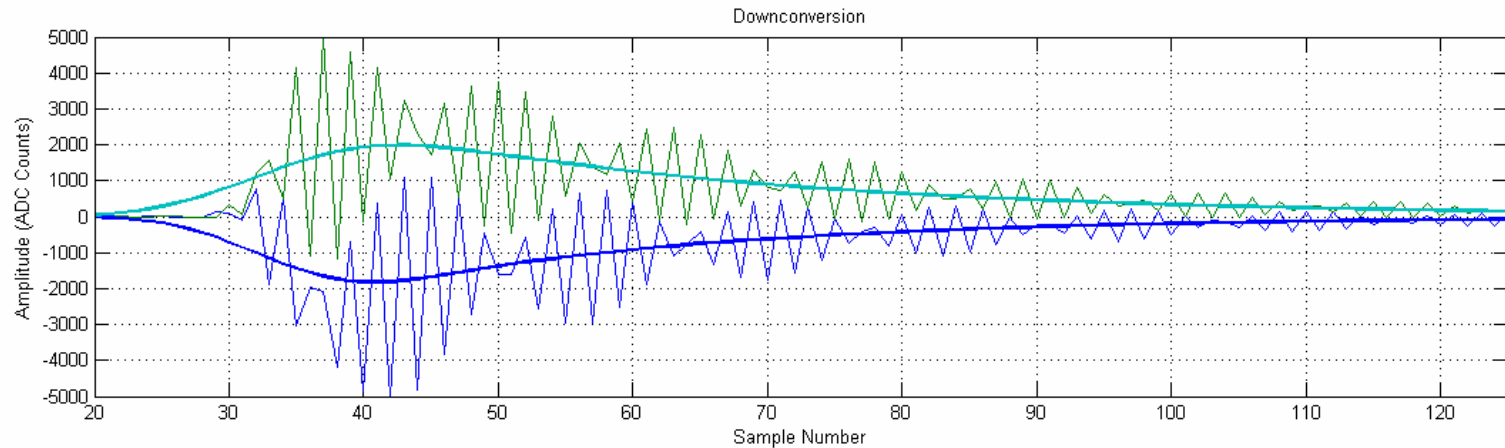
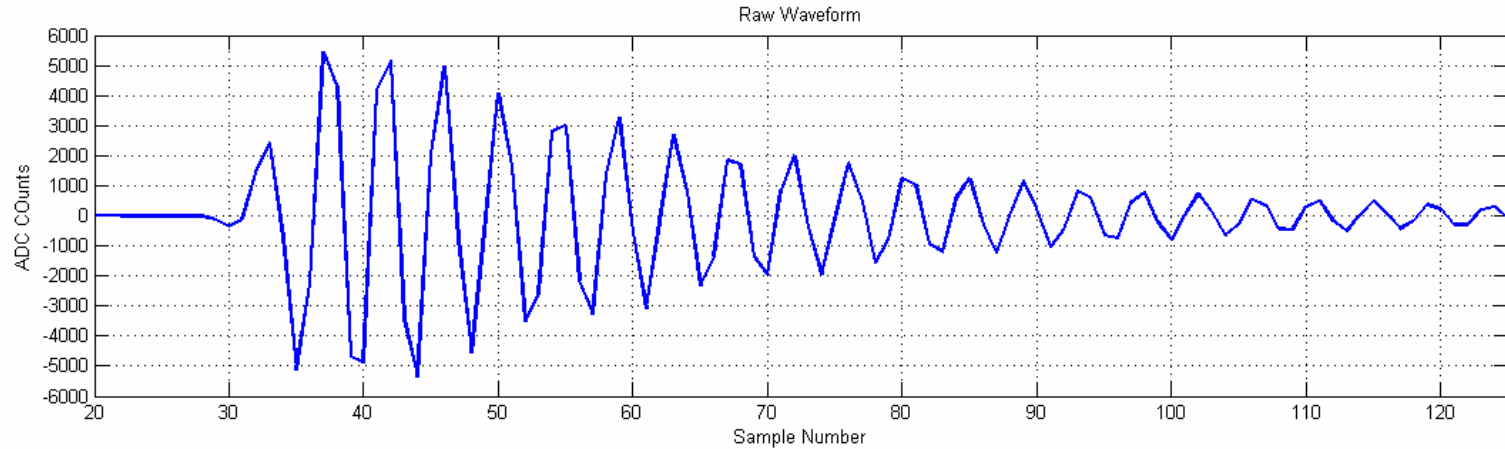
FIR Filter Coefficients

- Choose Finite Impulse Response (FIR) filter
 - Symmetric coefficients \rightarrow flat group delay



5.25685969697302E-05
1.6454424343439E-04
4.07154578172953E-04
8.72385025321259E-04
1.6766004340434E-03
2.95726074784519E-03
4.86225869836532E-03
7.53264980357207E-03
1.10807385993617E-02
1.55664596752274E-02
2.09756014054222E-02
2.72035613167032E-02
3.40479495420194E-02
4.12124906972027E-02
4.83233995659566E-02
5.49578635296309E-02
6.06826371814424E-02
6.50992446362904E-02
6.78910913982464E-02
6.88670806495452E-02
6.78910913982464E-02
6.50992446362904E-02
6.06826371814424E-02
5.49578635296309E-02
4.83233995659566E-02
4.12124906972027E-02
3.40479495420194E-02
2.72035613167032E-02
2.09756014054222E-02
1.55664596752274E-02
1.10807385993617E-02
7.53264980357207E-03
4.86225869836532E-03
2.95726074784519E-03
1.6766004340434E-03
8.72385025321259E-04
4.07154578172953E-04
1.6454424343439E-04
5.25685969697302E-05

Filter Downconverted Waveform

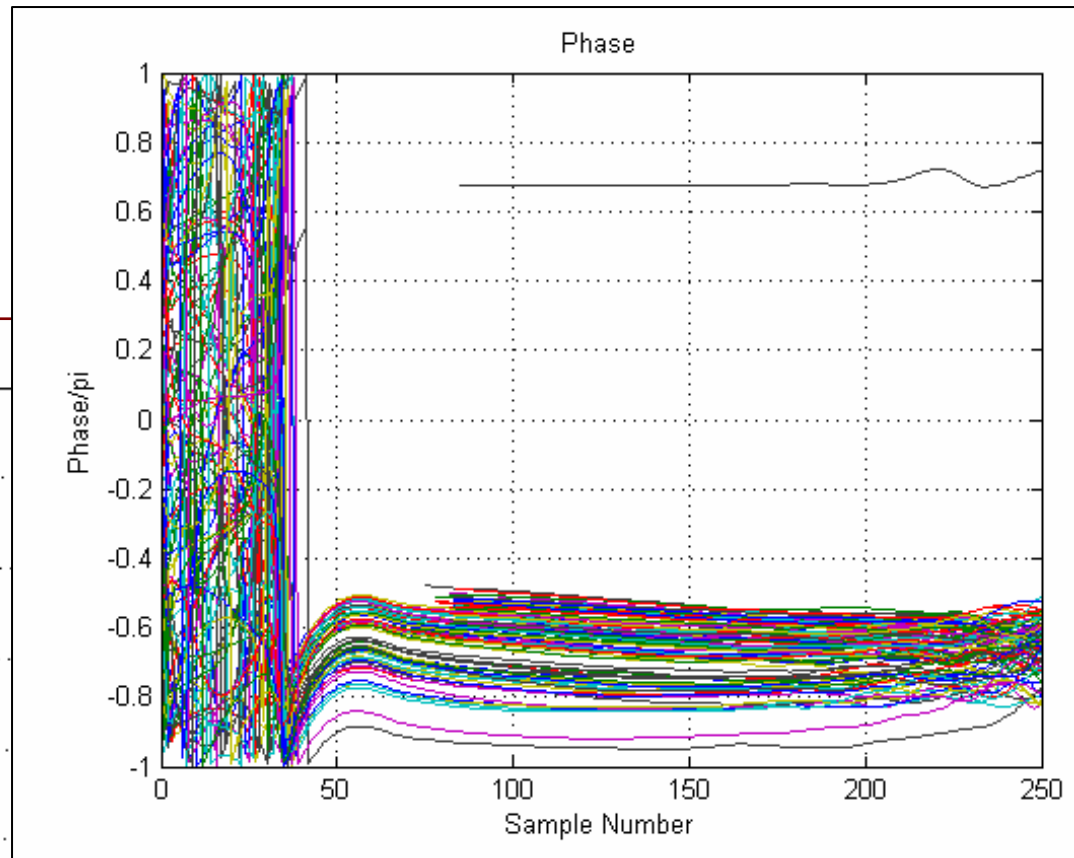
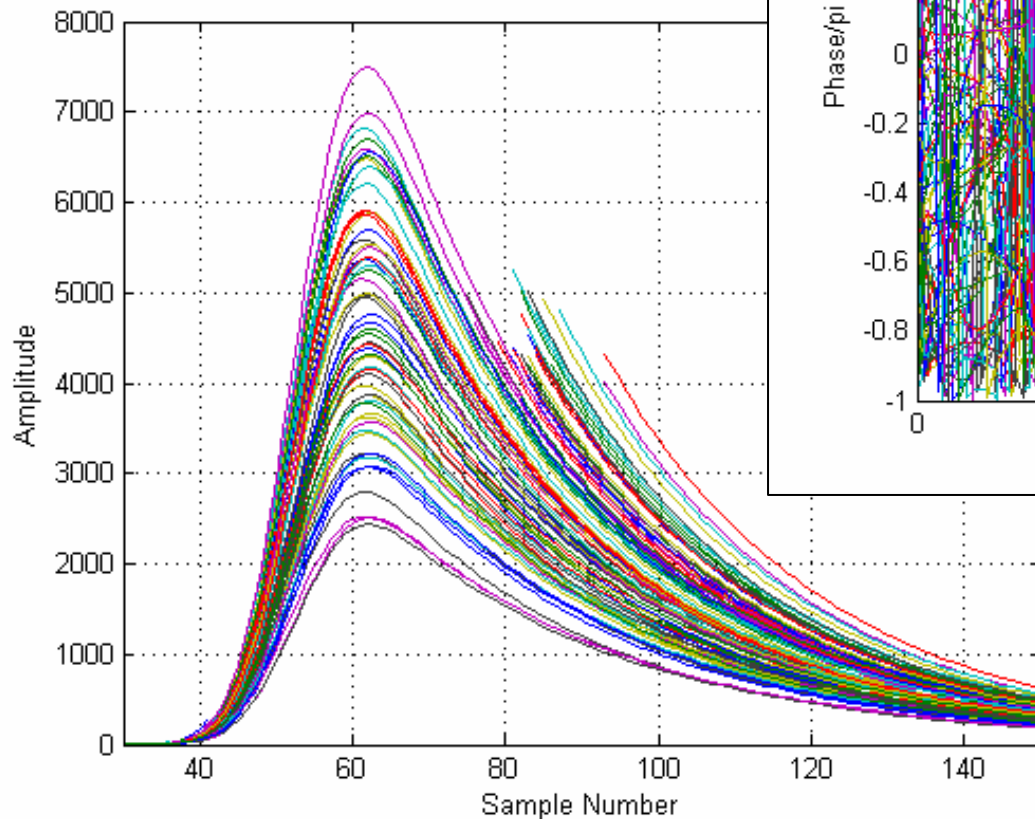


- Upper trace is Raw waveform
- Lower is demodulated waveform

Waveform Amplitude & Phase

Pick a time (sample number) at which to evaluate waveform amplitude & phase

Fixed sample time required to preserve linearity



Normalization

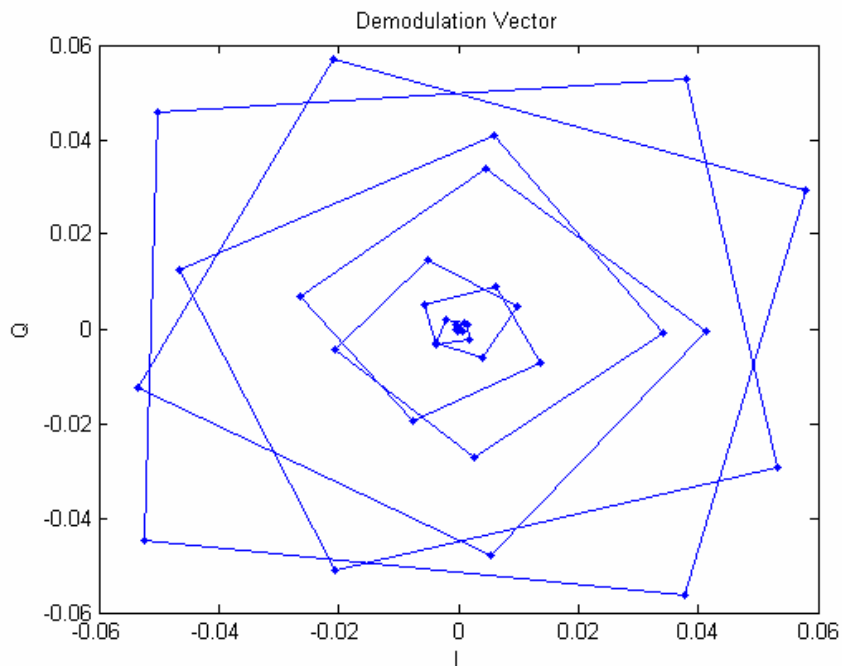
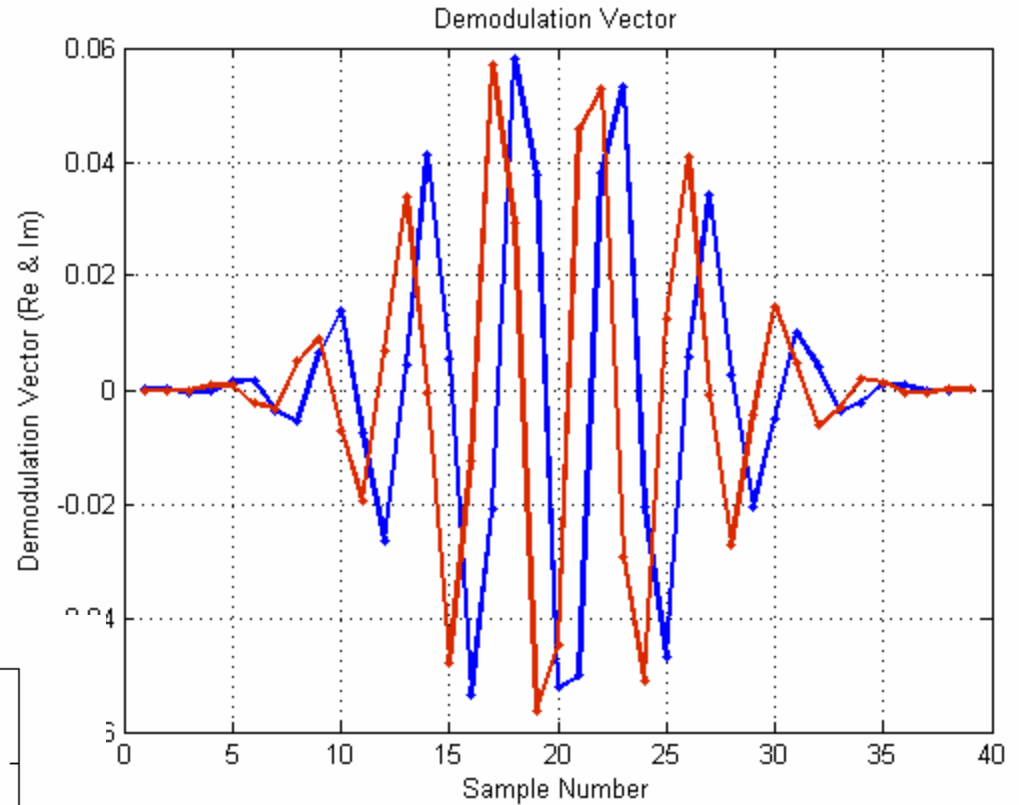
- Position cavity phase and amplitude are normalized to that of the reference cavity
- Divide (complex) position cavity amplitude by (complex) reference cavity amplitude
- Takes out charge and arrival phase of beam

Summary

1. Mix waveform with LO
i.e. frequency shift
 2. Lowpass filter
 3. Evaluate amplitude & phase at some fixed time
 4. Normalize to reference cavity amplitude & phase
 5. Shift, project out (position, tilt) components, & scale.
- Note that steps 1-3 above is numerically equivalent to taking the dot product of a vector of N_f elements with N_f digitized values of the cavity waveform where N_f is the length of the filter vector.

Demodulation Vector

- To get complex amplitude
- Dot this into equal length vector from cavity waveform



Saturation

- Many runs have few or no saturated pulses
 - (just ignore them?)
- My saturation algorithm:
 - Use first demodulated sample at or after nominal sample time uncontaminated by saturated ADC data
 - Correct phase using cavity frequency to roll back phase
 - Correct amplitude using decay constant to extrapolate amplitude back to nominal time.
- Not much study of how well this works.

Interfering Signals

- Sources:
 - Monopole Mode(s)
 - X-Y coupling
 - Pink (1/f) noise
 - Quadrupole modes
- What do they look like?
 - Time domain
 - Frequency domain
- How do they affect position measurement?
 - Quick answers;
 - Monopole mode => Fixed offset
 - X-Y coupling => linear transformation in (I,Q) space
 - Pink Noise => Suppressed by DDC
 - Quadrupole modes => Nonlinearity in (x,y) transfer function for large excursions

To Do

- Install Digital Downconversion in ROOT
- Approximately optimize
 - Filtering
 - Sample time
- Investigate handling of saturation
- Understand Calibration
- Should we establish DST files?
 - what format?